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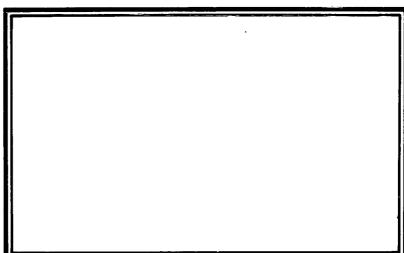


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TECHNICAL REPORT

MATERIAL LABORATORY
NEW YORK NAVAL SHIPYARD
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RESEARCH REPORT

on

THE THERMAL RADIATION CHARACTERISTICS OF NYLON FABRIC ASSEMBLIES

Submitted by
The Clothing Supply Office
(Research and Development Division)
U.S. Naval Supply Activities
Brooklyn, N.Y.

Lab. Project 5046-3, Part 96, Final Report

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Technical Objective AW-7

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SUMMARY

The thermal radiation characteristics of four nylon fabric assemblies, submitted by the Clothing Supply Office (Research and Development Division), U. S. Naval Supply Activities, Brooklyn, New York, have been evaluated. The critical thermal energies required for destruction of the fabric assemblies, were determined. The critical thermal energies required to produce a 2+ mild burn to skin behind the fabric were computed from the temperature rise of an underlying skin simulant attendant upon irradiation of the fabric assembly.

For the measurement of the critical thermal energies for cloth destruction the dynamic-exposure carbon-arc source with paraboloidal mirrors for collimating and condensing the emitted radiation was employed. The ll-mm static-exposure carbon-arc source with an ellipsoidal mirror for collecting and condensing the radiation was employed to determine the temperature-time characteristics of the polyethylene skin simulant behind the cloths. Using the temperature history measurements, the critical energies, corresponding to a 2+ mild burn undermeath the fabric assemblies were calculated.

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- 1 Critical Radiant Exposures of Fabric Assemblies
- 2 Exposures Required to Produce 2+ Mild Burn Behind Nylon Fabric Assemblies

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ADMINISTRATIVE INFORMATION

1. This investigation is part of the general Thermal Radiation program, proposed by Commander, New York Naval Shipyard confidential letter S99/L5, Serial 960-92, of 15 March 1950 and formally approved by Bureau of Ships speedletter S99-(0)(348), Serial 348-75, of 6 April 1950. The Thermal Radiation studies at the Naval Material Laboratory are under the supervision of the Armed Forces Special Weapons Project. This investigation was requested in Clothing Supply Office (Research and Development Division)letters 1D12-1:1g, A11/NT 53.01 of 4 March 1955 and 20 July 1955.

ACKNOWLEDG EMENTS

2. This investigation was planned and executed under the direction of T. I. Monahan, Supervisor of the Optics Section. W. L. Derksen furnished valuable assistance in the measurements involving the skin simulant.

INTRODUCTION

3. One of the major effects of atomic weapons on personnel arises from the instantaneous thermal radiation which may cause severe burns at relatively large distances from the center of the detonation. Studies carried out at the University of Rochester have indicated that the production of a so-called 2+ mild burn on uncovered porcine skin require, only 2.6 to 4.3 cal/cm² for rectangular impulses with emposure times of 0.1 to 1.0 seconds. (1) While clothing offers some protection to personnel by virtue of its insulating properties, the amount of heat transferred directly or by means of exothermic reactions by the clothing may result in a sufficient rise in temperature, to cause an incapacitating burn. A second degree burn in the human, corresponding to vesiculation, is sufficiently injurious and painful to be considered serious, if not incapacitating and it, therefore, has been adopted as the threshold for the production of casualties. As the energy required to produce 2+ burn in pig skin (spotty whiteness or coagulation) is comparable with that required to cause a second degree burn in humans, the 2+ pig-burn criterion is frequently applied when estimating the number of casualties in a given military situation.

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- 4. Previous studies conducted at the Naval Material Laboratory have indicated that variations in physical parameters (absorptance, nature of fiber material, weight of fabric) may alter considerably the resistance of fabrics to intense thermal radiation. (?) In addition to these parameters, which affect the damage to the cloths directly, physiological burns behind clothing are influenced by other physical factors, such as the thermal and optical constants of the skin and the transmittance and porosity of the fabrics. Recently laboratory methods for evaluating physiological burns behind fabrics, employing a plastic skin simulant, have been developed at the Naval Material Laboratory; the temperature history of the skin simulant behind an irradiated fabric system is measured and is interpreted in terms of the corresponding physiological burn, using methods developed at the Laboratory.
- 5. The Bureau of Supplies and Accounts, Department of the Navy, has assigned to the Clothing Supply Office (Research and Development Division); U. S. Naval Supply Activities, Brooklyn, New York, the responsibility for the development of garments designed to minimize the effects of the thermal radiation of nuclear weapons. In conjunction with this orogram, the Clothing Supply Office requested the Naval Material Laboratory to evaluate the thermal radiation characteristics of a group of four nylon fabric assemblies. The present report deals with the evaluation of these fabrics.

APPARATUS AND METHODS EMPLOYED

FABRIC ASSEMBLIES INVESTIGATED

6. For this evaluation, the Clothing Supply Office submitted four nylon fabric assemblies. The last two, designated as No. 14 and No. 15, consist of fabrics of the A-2 and A-1 cold weather uniforms of the Navy. The first assembly (No. 10b) consists of 3.5 oz. nylon twill, single coated neoprene, over knitted, 9.5 oz., nylon fleece and the second (No. 10b-1) the same two fabrics over waffle-knit cotton underwear.

CRITICAL THERMAL ENERGIES

7. The ll-mm dynamic-exposure carbon-arc source which utilizes two paraboloidal mirrors for collimating and condensing the emergent radiation was employed for the determination of the critical thermal energies of the fabric assemblies. The exposure times varied from 0.3 to 0.6 seconds for radiant exposures up to 53 cal/cm² and from 0.6 to 1.2 seconds for radiant exposures ranging from 53 to 106 cal/cm². The distribution of irradiance with time is essentially Gaussian, with time of maximum of irradiance approximately one-half the total exposure time. The maximum intensity of the source is 85 cal/cm² sec which is reduced by means of attenuating screens. The specimens were exposed to increasing amounts of thermal radiation until the first visual damage to the cloth surfaces was observed; the exposures were continued until at least the first fabric layer was completely destroyed, either during irradiance or as a result of afterflame.

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TRANSFER OF HEAT THROUGH CLOTHING

- 8. For determining the heat transfer through the clothing layers, specimens of the nylon fabric assemblies, 1.5 x 1.5 inches, were fastened on metal holders having a central, square aperture, 1-1/8 inches wide, mounted firmly, but with no tension, over the polyethylene skin simulant. To measure the temperature rise of the skin simulant, a thermocouple of No. 30 iron-constantan wire is imbedded in the center of this block at a depth of 0.023 cm. The temperature rise is indicated by a recording potentiometer. In the source employed for these measurements the carbon arc is mounted at the primary focus of an ellipsoidal mirror and fabric specimens are mounted at the secondary focus. The exposure time is controlled by a knife-bladed shutter mechanism, solenoid activated and energized by an electronic timer. The source irradiance is varied by means of attenuating screens.
- 9. The absorptance-corrected polyethylene skin simulant (4) was placed in contact with the various Tabric systems, but with no pressure applied, and the combination was irradiated at an irradiance level of 10 cal/cm² sec. The temperature histories obtained as a result of the irradiation of the cloth were analyzed by the methods outlined in the Naval Material Laboratory report on the development of the polyethylene skin simulant; (3) the radiant exposure to cause a 2+ mild burn was computed.

RESULTS

CRITICAL RADIANT EXPOSURES

- 10. The critical radiant exposures of the nylon fabric systems are given in Table 1. The significant data are summarized as follows:
 - a. Initial Effects. The three assemblies with an outer layer of nylon twill, designated as 10b, 10b-1 and 15, showed initial damage, consisting of melting, after exposures of 5.6, 6.7 and 8.5 cal/cm², respectively. The outer cotton layer of the fourth assembly, (No. 14) was charred at a radiant exposure of 11 cal/cm².
 - b. Destruction of First Layer. The destruction of the outer layer of the cotton fabric in the A-2 cold weather combination, coincided with destruction of the second layer of this assembly and occurred at a radiant exposure of 18 cal/cm². The destruction of the outer-layers of assemblies 10b, 10t-1 and 15 occurred at 12, 14, and 18 cal/cm² respectively.
 - c. Flaming During Exposure. The three assemblies with nylon outerlayers (10b, 10b-1, 15) flamed during exposure to approximately 55 cal/cm².

(3)(4)	Bibliography
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- d. Destruction of Nylon Fleece. The nylon fleece, forming the second layer with nylon surface layers, 15, 10b and 10b-1, melted through at 68, 75, and 84 cal/cm² respectively.
- e. Additional Layers. The third layer of the A-1 cold weather combination was destroyed after exposure to 83 cal/cm². The cotton waffle knit underwear, torming the innermost layer of the two cold-weather combinations, remained undamaged, even when irradiated by a radiant exposure of 106 cal/cm².

TRANSFER OF HEAT THROUGH CLOTHING

- 11. The radiant exposures required to produce a 2+ mild burn under the fabric assemblies, are listed in Table 2. Details of the results are discussed below.
 - a. Two-layer Assembly. The temperature histories measured under the only two-layer nylon assembly investigated (10b) indicate that a 2+ mild burn is to be expected after a radiant exposure of 30 cal/cm².
 - b. Three-layer Assemblies. The two three-layer assemblies evaluated 10b-1 and 14, require 65 and 56 cal/cm², respectively, to cause a 2+ mild burn. The addition of the waffle-knit to the two-layer assembly above causes an increase in the radiant exposure for a 2+ mild burn from 30 to 65 cal/cm². On the other hand, replacement of the top layer, consisting of neoprene coated nylon twill, by cotton exford causes a reduction in the required radiant exposure for a 2+ mild burn from 65 to 56 cal/cm²; this assembly was the only one of the four investigated which sustained afterflame.
 - c. Six-layer Assembly. For a radiant exposure of 127 cal/cm² the temperature rise under the A-1 cold weather combination, designated as 15, the temperature rise was only 12°C; this rise is considerably lower than that required to produce a 2+ mild burn under this combination of layers.
 - d. Hazard of Molten Nylon During the investigation of the nylon fabric assemblies, it was observed that heated nylon fabric forms a melt which produces an instantaneous and painful burn as soon as it comes in contact with uncovered skin. The molten material adheres strongly to human skin. The relatively low critical radiant exposure required for destruction of the outer nylon fabrics indicates an additional hazard of this fabric, particularly where the cloth comes in direct contact with the skin.

ANALYSIS

- 12. leview of the experimental findings indicates the following trends:
 - a. As compared to cotton, the nylon fabrics are more vulnerable to effects of thermal radiation.

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- b. As would be expected, thermal radiation damage to skin is considerably reduced with an increase in the number of layers of clothing. The six layer assembly, when not destroyed, offers excellent protection against burns resulting from thermal transfer through the layers. It should be noted that the accuracy of the data for the multilayer assemblies is doubtful as the number of layers is increased, because of the limited area of irradiation relative to the thickness of the assembly.
- c. Because molten nylon causes severe burns on uncovered skin and because nylon fabrics are rather easily affected by incident thermal radiation, nylon fabrics present a particular hazard when employed in surface layers and in contact with unprotected skin areas (hands, face etc.)
- d. Since cotton in contact with an underlying layer of nylon was found to cause destruction of the nylon layer simultaneously with its own destruction, the resistance of nylon under cotton is low.

CONCLUSIONS

- 13. The following conclusions may be drawn from the results of this study:
 - a. The amount of protection offered by a single layer of the nylon fabrics investigated is small, since these layers show initial effects after exposures to less than 9 cal/cm² and destruction after exposures to less than 18 cal/cm².
 - b. It was observed that flames develop during radiant exposures of approximately 55 cal/cm² on the nylon fabric assemblies.
 - c. The numerous layers contained in the cold weather combinations provide considerable protection against thermal radiation hazards. The last layer of these assemblies, consisting of cotton waffle knit underwear, remained undamaged up to a radiant exposure of 106 cal/cm². An exposure of 127 cal/cm² did not cause a 2+ mild burn under the A-l cold weather combination.
 - d. A 2+ mild burn may be expected after exposure to 30 cal/cm² on one of the two layer assemblies (No. 10b). The same burn occurs after 56 cal/cm² under the first three-layers assembly (No. 14) and after 65 cal/cm² under the second three-layer assembly (No. 10b-1).

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e. If molten nylon, such as produced in radiation exposures, comes in contact with bare skin, it will produce instantaneous and painful ourns and can only be removed with difficult...

Approved:

JONES Jr., CAN The Director

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TABLE 1

CRITICAL RADIANT EXPOSURES OF CLOTHING ASSEMBLIES
U. S. Naval Supply Activities, Brocklyn, N. I., Department of the Navy

NEA Description of Clothing Assembly Conter surface begins to low count, single coated Clothing Assembly Court layer melted through Neoprene; 9.5 oz. Nylon Twill, low Count, single coated Cotton Waffle-Knit underwear Cotton				
ignation Clothing Assembly 3.5 oz. Nylon twill Low count, single coated Neoprene; 9.5 oz. Nylon Fleece, Knitted o.5 oz. Nylon Twill, low count, single coated Neoprene; 9.5 oz. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear A-2 Cold Keather Combination; 9.0 oz. Cotton Oxford, 9.5 oz. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Keather Combination; 3.5 oz. Nylon Fleece, Cotton Vafile Soz. Nylon Soz. Nylon Fleece; 1.8 oz. Nylon Fleece; 1.8 oz. Nylon Fleece; 1.8 oz. Nylon Fleece; 1.8 oz. Nylon Fuill; Acetate Batting; 1.8 oz. Nylon Twill Cotton Waffle-Knit Underwear	MSA	Description of		Critical
Low count, single coated Neoprene; 9.5 oz. Nylon Fleece, Knitted 3.5 oz. Nylon Twill, low count, single coated Neoprene; 9.5 oz. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear A-2 Cold Keather Combination; 9.0 oz. Cotton Oxford, 9.5 oz. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combination; 3.5 oz. Nylon Twill 9.5 oz. Nylon Fleece; 1.8 oz. Nylon Fleece; 1.8 oz. Nylon Fwill; Acetate Batting; 1.8 oz. Nylon Twill Cotton Waffle-Knit Underwear	Designation	Clothing Assembly	Description of Effect	Exposure (cal/cm ²)
Neoprene; 9.5 oz. Nylon Fleece, Knitted count, single coated Neoprene; 9.5 os. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear tion; 9.0 oz. Cotton Oxford, 9.5 oz. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combination; 3.5 oz. Nylon Fuill 9.5 oz. Nylon Fuill 9.5 oz. Nylon Fuill 0.5 oz. Nylon Fleece; 1.8 oz. Nylon Fuill; Acetate Batting; 1.8 oz. Nylon Fuill Cotton Waffle-Knit Underwear	106		Onter surface begins to	5.6
Fleece, Knitted 3.5 oz. Nylon Twill; low count, single coated Neoprene; 9.5 os. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear A-2 Cold Keather Conbination; 9.0 oz. Cotton Oxford, 9.5 oz. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combination; 3.5 oz. Nylon Twill 9.5 oz. Nylon Fleece; 1.8 os. Nylon Twill; Acetate Batting; 1.8 oz. Nylon Twill Cotton Waffle-Knit Underwear		Neoprene: 9.5 oz. Nylon	Outer layer melted through	71
count, single coated Neoprene; 9.5 os. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear A-2 Cold Weather Combination; 9.0 oz. Cotton Oxford, 9.5 oz. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combination; 3.5 oz. Nylon Fwill 9.5 oz. Nylon Fleece; 1.8 os. Nylon Friece; 1.8 os. Nylon Friece; 1.8 os. Nylon Friece; 1.8 os. Nylon Friece; 1.8 cotton Waffle-Knit Underwear		Fleece, Kni tted	Top surface of Nylon Fleece	
count, single coated Neoprene; 9.5 os. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear A-2 Cold Keather Combination; 9.0 oz. Cotton Oxford, 9.5 oz. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combination; 3.5 oz. Nylon Twill 9.5 oz. Nylon Fleece; 1.8 os. Nylon Twill; Acetate Batting; 1.8 oz. Nylon Twill Cotton Waffle-Knit Underwear			begins to nelt	7 <u>7</u>
count, single coated Neoprene; 9.5 os. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear A-2 Cold Keather Combins- tion; 9.0 os. Cotton Oxford, 9.5 os. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combins- tion; 3.5 os. Nylon Twill 9.5 os. Nylon Fleece; 1.8 os. Nylon Twill; Acetate Batting; 1.8 os. Nylon Twill Cotton Kaffle-Knit Underwear	•		Flames during exposure	
count, single coated Neoprene; 9.5 os. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear A-2 Cold Keather Combins- tion; 9.0 os. Cotton Oxford, 9.5 os. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combins- tion; 3.5 os. Nylon Twill 9.5 os. Nylon Fleece; 1.8 os. Nylon Twill; Acetate Batting; 1.8 os. Nylon Twill Cotton Kaffle-Knit Underwear			Nylon Fleece melted through	75
count, single coated Neoprene; 9.5 os. Nylon Fleece, Knitted; Cotton Waffle-Knit underwear tion; 9.0 oz. Cotton Oxford, 9.5 oz. Nylon Fleece, Cotton Waffle-Knit underwear A-1 Cold Weather Combina- tion; 3.5 oz. Nylon Fwill 9.5 oz. Nylon Fleece; 1.8 os. Nylon Fleece; 1.8 os. Nylon Full; Acetate Batting; 1.8 oz. Nylon Twill Cotton waffle-Knit Underwear	100-1	3.5 oz. Nylon Twill, low	Outer surface begins to melt	6.7
	1	count, single coated Neoprene;	Outer layer melted through	큐
		9.5 os. Nylon Fleece, Knitted;	Top surface of Nylon He ece	•
I H		Cotton Waffle-Knit underwear	begins to melt	% :
II H			Flames during exposure	ኤ
13 H			Nylon Fleece melted through	2
ជ ង		A-2 Cold keather Combina-	Cotton outer layer charred	#
ជង	•	tion; 9.0 oz. Cotton	Outer layer & Nylon Fleece	
ជង		Oxford, 9.5 oz. Nylon	destroyed by after flame	•
ជង		Fleece, Cotton Waffle-Knit	& after glow	18
ជង		underwear		
ជ ង	E5	A-1 Cold Weather Combina-	Nylon Twill outer layer begins	,
ជាង		tion; 3.5 os. Nylon Twill	to melt	8 5 1
ជង		9.5 oz. Mylon Fleece; 1.8	Outer layer melted through	2
ជ ង		os. Nylon Twill; Acetate	Flames during exposure	₹
le-Knit Underwear		Batting; 1.8 oz. Wylon Twill	Top surface of Nylon Fleece	
Nylon Fleece melts through Third layer (1.8 oz. Nylon Twill)melts through;		Cotton kaffle-Knit Underwear	begins to melt	<u>ස</u>
Third layer (1.8 oz. Nylon Twill)melts through;	-		Nylon Fleece melts through	8
INIII/metcs dirough;			Third layer (1.8 oz. Nylon	6
			TWILL/metrs unrough;	20

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TABLE 2

EXPOSURES REQUIRED TO PROPUGE 2+ MILD FURNS UNDER FARRIC ASSEMBLIES

submitted by U. S. Naval Supply Activities, Brooklyn, New York, Department of the Navy

								22	COMPUTED
	No.				Temp.		Duration Crit.	Crit	
Assembly	of Time Layers (sec)	Time (sec)	<pre>Trradiance (cal/cm² sec.)</pre>	Exposure (cal/cm^2)	(°C)	Eifect on Fabric	temp. (sec)	e se O	$2+3i1d$ Burn $(ca1/cm^2)$
10b	2	2.72	11.7	31.8	8	Bu rned Through	16	37	30
100-1	m	5.00	12.2	61.2	æ	2 layers Eurned through	33	e E	65
7	m	4.53	12.3	55.1	Ж	Afterflame & Afterglow	22	×	56
15	9	10.0	12.7	127	12	Afterglow 4th layer Charred	142	S.	> 250

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